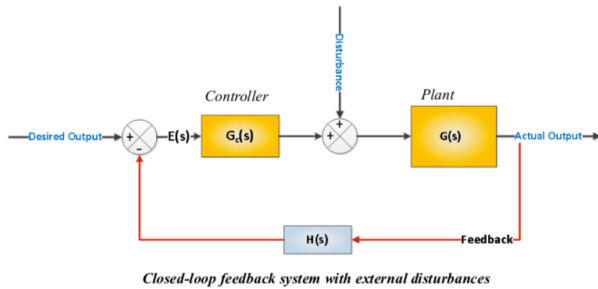


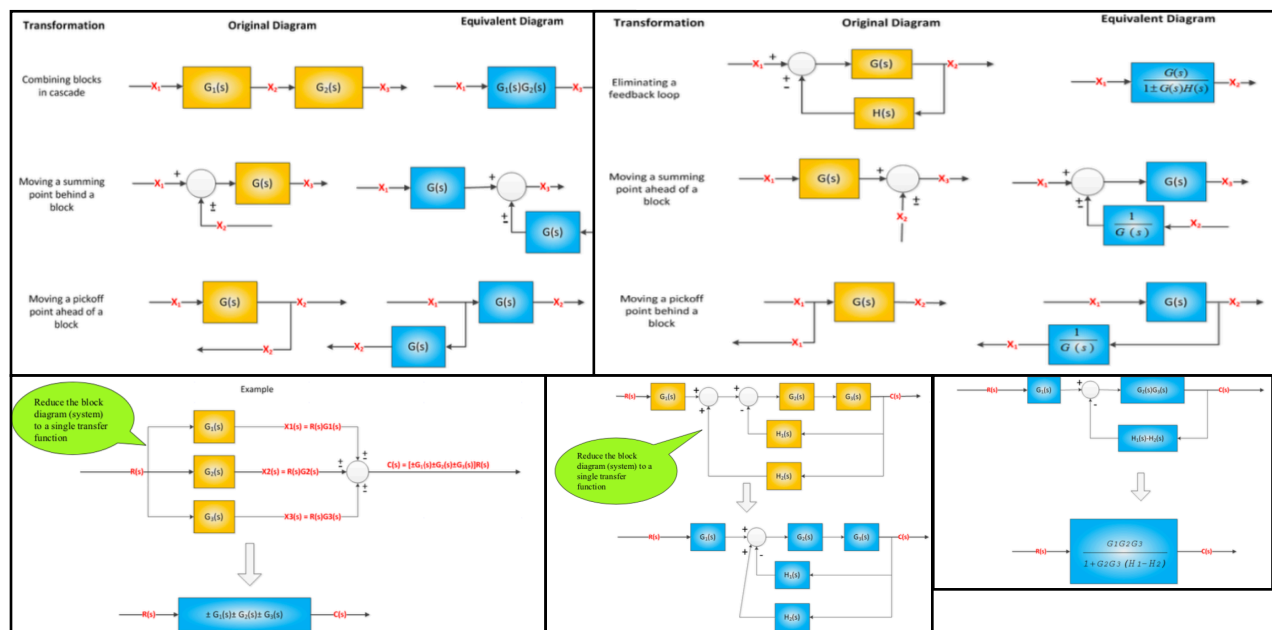
# Week5 - Effects of Disturbances

- One of the advantages of the closed-loop systems over the open-loops systems is the ability to reject external disturbances, and measurement noise.
- External disturbances
  - Are always present (at some degree) in real world applications
  - Must be accounted for in practical closed-loop systems



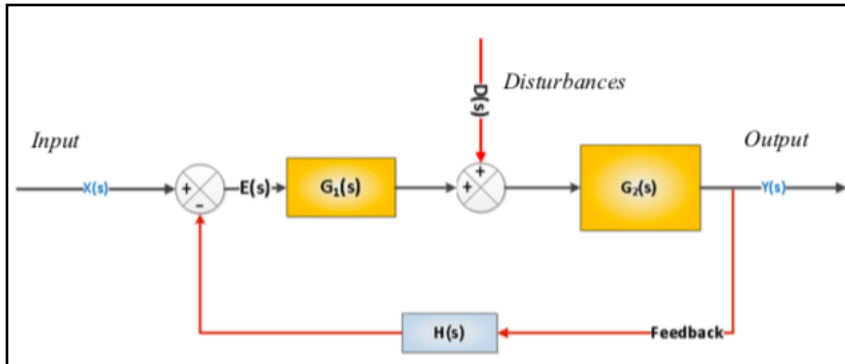
## Block Diagram Reduction

- Block diagram reduction techniques
  - Purpose:
    - To be able to re-arrange, reduce, and analyze block diagrams of different systems, involving disturbances (and other) effects
    - To better understand the disturbance effects in control systems
  - Blocks can be connected in series only if the output of one block is not affected by the next following block
  - If there are loading effects between components it is necessary to combine these components into a single block
  - Cascaded block representing non-loading components can be replaced by a single block
  - Complicated block diagrams involving many feedback loops can be simplified using step-by-step approach (ie., rearrangement using rules of block diagram algebra)

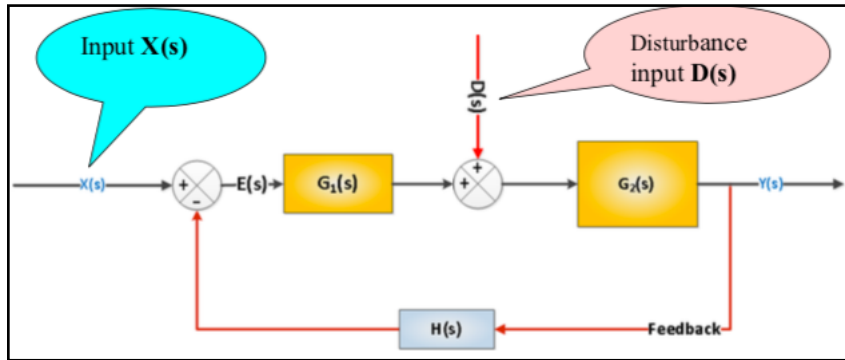


## The Effect of Disturbances

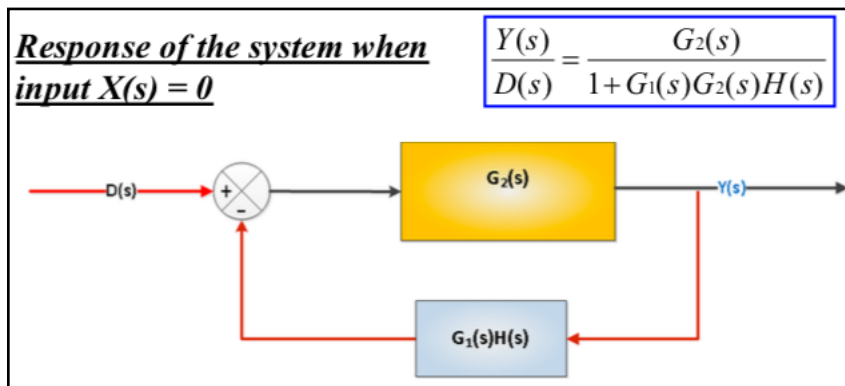
- Closed loop system in a presence of disturbances



- Expressing the output  $Y(s)$  in terms of input  $X(s)$  and disturbance  $D(s)$  we use **superposition**
- For linear systems: response to several inputs can be calculated by treating one input at a time and adding the results.
- Let us illustrate the application of superposition principle in this example



- Applying superposition enables us to treat one input at a time:



- The final outcome of the system in the presence of the input  $X(s)$  and disturbance  $D(s)$  is obtained by adding both responses:

$$Y(s) = \frac{G_2(s)}{1 + G_1(s)G_2(s)H(s)} D(s) + \frac{G_1(s)G_2(s)}{1 + G_1(s)G_2(s)H(s)} X(s)$$

$$Y(s) = [D(s) + G_1(s)X(s)] \left[ \frac{G_2(s)}{1 + G_1(s)G_2(s)H(s)} \right]$$

Consider the case when:

$$G_1(s)G_2(s)H(s) \gg 1 \quad \text{and} \quad G_1(s)H(s) \gg 1$$

$$Y(s) = [D(s) + G_1(s)X(s)] \left[ \frac{G_2(s)}{G_1(s)G_2(s)H(s)} \right]$$

$$Y(s) = [D(s) + G_1(s)X(s)] \left[ \frac{1}{G_1(s)H(s)} \right]$$

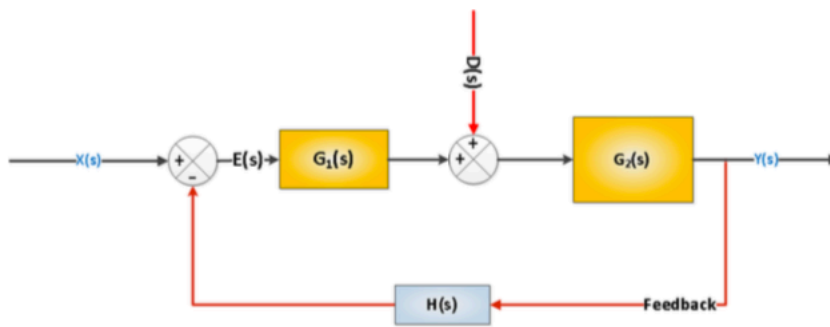
When  $H(s) = 1$  we can see that the output  $Y(s)$  follows the input  $X(s)$ ...and The effect of the disturbance  $D(s)$  is suppressed!

$$Y(s) = \cancel{[D(s) + G_1(s)X(s)]} \left[ \frac{1}{G_1(s)H(s)} \right] = X(s) \frac{1}{H(s)}$$

Negligible since  $G_1(s)H(s) \gg 1$

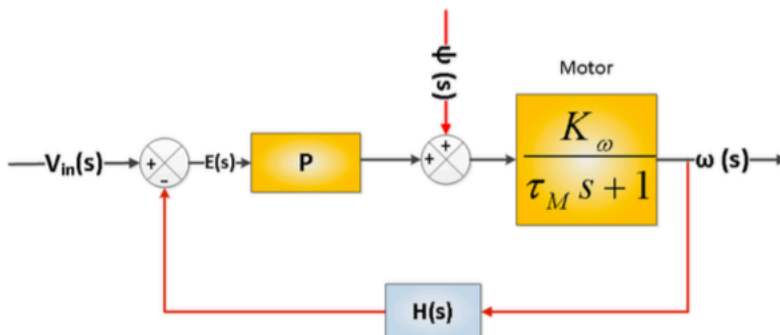
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## Example:



Let's adapt the general example of the closed-loop system in a presence of disturbances to a DC motor...

$$X(s) = V_{in}(s) \quad Y(s) = \omega(s) \quad D(s) = \psi(s) \quad G_1 = P \quad G_2 = \frac{K_\omega}{\tau_M s + 1}$$



Let's adapt the general example of the closed-loop system in a presence of disturbances to a DC motor...

$$X(s) = V_{in}(s) \quad Y(s) = \omega(s) \quad D(s) = \psi(s) \quad G_1 = P$$

$$Y(s) = [D(s) + G_1(s)X(s)] \left[ \frac{G_2(s)}{1 + G_1(s)G_2(s)H(s)} \right]$$

$$\omega(s) = [\Psi(s) + PV_{in}(s)] \left[ \frac{\frac{K_\omega}{\tau_M s + 1}}{1 + P \frac{K_\omega}{\tau_M s + 1} H(s)} \right]$$

➔ 
$$\omega(s) = [\Psi(s) + PV_{in}(s)] \left[ \frac{K_\omega}{\tau_M s + 1 + PK_\omega H(s)} \right]$$

□ Final value of the output is reached when

■  $t \rightarrow \infty$  or  $s \rightarrow 0$ , thus we have:

$$\lim_{s \rightarrow 0} \omega(s) = \lim_{s \rightarrow 0} [\Psi(s) + PV_{in}(s)] \left[ \frac{K_\omega}{\tau_M s + 1 + PK_\omega H(s)} \right]$$

0

➔ 
$$\omega(s)_{Steady-state} = [\Psi(s) + PV_{in}(s)] \left[ \frac{K_\omega}{1 + PK_\omega H(s)} \right]$$

➔ 
$$\omega(s)_{Steady-state} = \underbrace{[\Psi(s)]}_{\text{Disturbance effect}} + \underbrace{[PV_{in}(s)]}_{\text{SetPoint effect}} \left[ \frac{K_\omega}{1 + PK_\omega H(s)} \right]$$

$$\omega(s)_{Steady-state} = \underbrace{\Psi(s) \frac{K_\omega}{1 + PK_\omega H(s)}}_{\text{Disturbance effect}} + \underbrace{V_{in}(s) \frac{PK_\omega}{1 + PK_\omega H(s)}}_{\text{SetPoint effect}}$$

*Final outcome of a DC motor system in the presence of disturbances*

- Let's analyze the final outcome of a DC motor system in the presence of input  $V_{in}$  and disturbances  $\psi$

The diagram shows the steady-state angular velocity  $\omega(s)_{Steady-state}$  as the sum of two terms. The first term, labeled 'Disturbance effect', is  $\Psi(s) \frac{K_\omega}{1 + PK_\omega H(s)}$  and is highlighted in a pink box. A red arrow points from the text 'Disturbance effect' to this term. The second term, labeled 'SetPoint effect', is  $V_{in}(s) \frac{PK_\omega}{1 + PK_\omega H(s)}$  and is highlighted in a blue box. A blue arrow points from the text 'SetPoint effect' to this term.

$$\omega(s)_{Steady-state} = \Psi(s) \frac{K_\omega}{1 + PK_\omega H(s)} + V_{in}(s) \frac{PK_\omega}{1 + PK_\omega H(s)}$$

As proportional gain P or H is increased  $\rightarrow \psi$  decreases  
 $\psi$  becomes negligible, however is never completely eliminated

**Remarks:**

- In order to compensate for the effect of disturbances, we can compensate by adding an offset to the SetPoint, whereas the offset amount is such as to cancel the disturbance effect...
- The above offset technique will not work in the presence of changing (variable) disturbances
- Use of better (more efficient) techniques shall be investigated at a later time